

In cylindrical coordinates, $\mathbf{v} = v_r \mathbf{e}_r + v_\theta \mathbf{e}_\theta + v_z \mathbf{e}_z$. Use the expressions

$$\nabla = \left(\frac{\partial}{\partial r}, \frac{1}{r} \frac{\partial}{\partial \theta}, \frac{\partial}{\partial z} \right)$$

and

$$\nabla^2 = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\partial^2}{\partial z^2}$$

to derive the three components of the momentum equation

$$(\mathbf{v} \cdot \nabla) \mathbf{v} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v}.$$

In the derivation, note that

$$\frac{\partial \mathbf{e}_r}{\partial \theta} = \mathbf{e}_\theta \quad \text{and} \quad \frac{\partial \mathbf{e}_\theta}{\partial \theta} = -\mathbf{e}_r.$$

$$\bar{\mathbf{v}} \cdot \nabla = v_r \frac{\partial}{\partial r} + \frac{v_\theta}{r} \frac{\partial}{\partial \theta} + v_z \frac{\partial}{\partial z}$$

$$(\bar{\mathbf{v}} \cdot \nabla)(v_r \bar{\mathbf{e}}_r) = \left(v_r \frac{dv_r}{dr} + \frac{v_\theta}{r} \frac{dv_r}{d\theta} + v_z \frac{dv_r}{dz} \right) \bar{\mathbf{e}}_r + \frac{v_\theta v_r}{r} \bar{\mathbf{e}}_\theta$$

$$(\bar{\mathbf{v}} \cdot \nabla)(v_\theta \bar{\mathbf{e}}_\theta) = \left(v_r \frac{dv_\theta}{dr} + \frac{v_\theta}{r} \frac{dv_\theta}{d\theta} + v_z \frac{dv_\theta}{dz} \right) \bar{\mathbf{e}}_\theta - \frac{v_\theta^2}{r} \bar{\mathbf{e}}_r$$

$$(\bar{\mathbf{v}} \cdot \nabla)(v_z \bar{\mathbf{e}}_z) = \left(v_r \frac{dv_z}{dr} + \frac{v_\theta}{r} \frac{dv_z}{d\theta} + v_z \frac{dv_z}{dz} \right) \bar{\mathbf{e}}_z$$

$$\frac{1}{r} \frac{d}{dr} \left(r \frac{d}{dr} \right) \bar{\mathbf{v}} = \frac{1}{r} \frac{d}{dr} \left(r \frac{dv_r}{dr} \right) \bar{\mathbf{e}}_r + \frac{1}{r} \frac{d}{dr} \left(r \frac{dv_\theta}{dr} \right) \bar{\mathbf{e}}_\theta + \frac{1}{r} \frac{d}{dr} \left(r \frac{dv_z}{dr} \right) \bar{\mathbf{e}}_z$$

$$\frac{d}{d\theta} (v_r \bar{\mathbf{e}}_r + v_\theta \bar{\mathbf{e}}_\theta + v_z \bar{\mathbf{e}}_z) = \left(\frac{dv_r}{d\theta} - v_\theta \right) \bar{\mathbf{e}}_r + \left(\frac{dv_\theta}{d\theta} + v_r \right) \bar{\mathbf{e}}_\theta + \frac{dv_z}{d\theta} \bar{\mathbf{e}}_z$$

$$\frac{1}{r^2} \frac{d^2}{d\theta^2} (\bar{\mathbf{v}}) = \frac{1}{r^2} \left(\frac{d^2 v_r}{d\theta^2} - 2 \frac{dv_\theta}{d\theta} - v_r \right) \bar{\mathbf{e}}_r + \frac{1}{r^2} \left(\frac{d^2 v_\theta}{d\theta^2} + 2 \frac{dv_r}{d\theta} - v_\theta \right) \bar{\mathbf{e}}_\theta + \frac{d^2 v_z}{r^2 d\theta^2} \bar{\mathbf{e}}_z$$

$$\frac{d^2 \bar{\mathbf{v}}}{d\theta^2} = \frac{d^2 v_r}{d\theta^2} \bar{\mathbf{e}}_r + \frac{d^2 v_\theta}{d\theta^2} \bar{\mathbf{e}}_\theta + \frac{d^2 v_z}{d\theta^2} \bar{\mathbf{e}}_z$$

$$r: \quad \frac{dv_r}{dt} + v_r \frac{dv_r}{dr} + \frac{v_\theta}{r} \frac{dv_r}{d\theta} + v_z \frac{dv_r}{dz} - \frac{v_\theta^2}{r} = -\frac{1}{\rho} \frac{\partial p}{\partial r} + \nu \left[\frac{1}{r} \frac{d}{dr} \left(r \frac{dv_r}{dr} \right) - \frac{v_r}{r^2} + \frac{1}{r^2} \frac{d^2 v_r}{d\theta^2} - \frac{2}{r^2} \frac{dv_\theta}{d\theta} + \frac{d^2 v_r}{dz^2} \right]$$

$$\frac{d}{dr} \left(\frac{1}{r} \frac{d}{dr} (rv_r) \right)$$

$$\theta: \quad \frac{dv_\theta}{dt} + v_r \frac{dv_\theta}{dr} + \frac{v_\theta}{r} \frac{dv_\theta}{d\theta} + v_z \frac{dv_\theta}{dz} + \frac{v_\theta v_r}{r} = -\frac{1}{\rho} \frac{1}{r} \frac{\partial p}{\partial \theta} + \nu \left[\frac{1}{r} \frac{d}{dr} \left(r \frac{dv_\theta}{dr} \right) - \frac{v_\theta}{r^2} + \frac{1}{r^2} \frac{d^2 v_\theta}{d\theta^2} + \frac{2}{r^2} \frac{dv_r}{d\theta} + \frac{d^2 v_\theta}{dz^2} \right]$$

$$\frac{d}{dr} \left(\frac{1}{r} \frac{d}{dr} (rv_\theta) \right)$$

$$z: \quad \frac{dv_z}{dt} + v_r \frac{dv_z}{dr} + \frac{v_\theta}{r} \frac{dv_z}{d\theta} + v_z \frac{dv_z}{dz} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + \nu \nabla^2 v_z$$

For axisymmetric flow $\mathbf{v} = v_r(r, z)\mathbf{e}_r + v_z(r, z)\mathbf{e}_z$ show that

$$\boldsymbol{\omega} = \nabla \wedge \mathbf{v} = \omega_\theta \mathbf{e}_\theta = \left(\frac{\partial v_r}{\partial z} - \frac{\partial v_z}{\partial r} \right) \mathbf{e}_\theta.$$

If the flow is inviscid, show that the vorticity equation reduces to

$$\frac{D}{Dt} \left(\frac{\omega_\theta}{r} \right) = \frac{\partial}{\partial t} \left(\frac{\omega_\theta}{r} \right) + v_r \frac{\partial}{\partial r} \left(\frac{\omega_\theta}{r} \right) + v_z \frac{\partial}{\partial z} \left(\frac{\omega_\theta}{r} \right) = 0.$$

$$\boldsymbol{\omega} = \frac{1}{r} \begin{vmatrix} \bar{\mathbf{e}}_r & r\bar{\mathbf{e}}_\theta & \bar{\mathbf{e}}_z \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ v_r(r, z) & r\dot{\theta} & v_z(r, z) \end{vmatrix} = \left(\frac{\partial v_r}{\partial z} - \frac{\partial v_z}{\partial r} \right) \bar{\mathbf{e}}_\theta$$

$$\frac{D}{Dt} \bar{\boldsymbol{\omega}} = (\bar{\boldsymbol{\omega}} \cdot \nabla) \bar{\mathbf{v}} \Rightarrow \frac{\partial \bar{\boldsymbol{\omega}}}{\partial t} + (\bar{\mathbf{v}} \cdot \nabla) \bar{\boldsymbol{\omega}} = (\bar{\boldsymbol{\omega}} \cdot \nabla) \bar{\mathbf{v}}$$

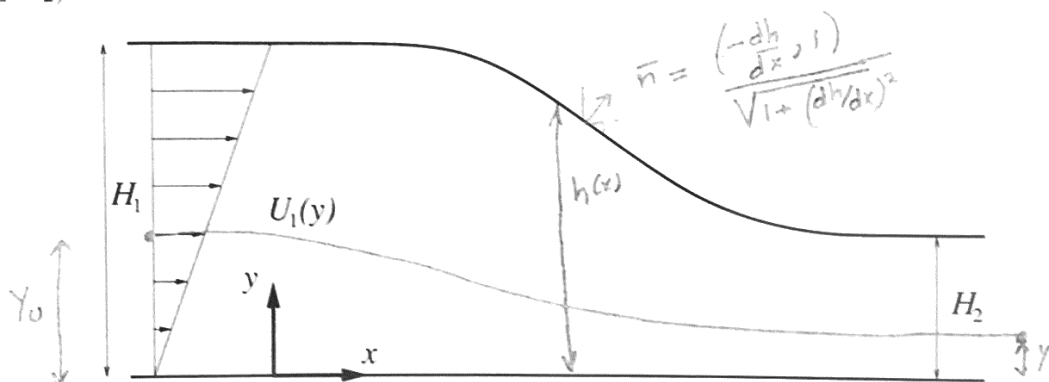
$$\bar{\mathbf{v}} \cdot \nabla = v_r \frac{\partial}{\partial r} + v_z \frac{\partial}{\partial z} \Rightarrow (\bar{\mathbf{v}} \cdot \nabla) \bar{\boldsymbol{\omega}} = \left(v_r \frac{\partial \omega_\theta}{\partial r} + v_z \frac{\partial \omega_\theta}{\partial z} \right) \bar{\mathbf{e}}_\theta$$

$$\bar{\boldsymbol{\omega}} \cdot \nabla = \frac{\omega_\theta}{r} \frac{\partial}{\partial \theta} \Rightarrow (\bar{\boldsymbol{\omega}} \cdot \nabla) \bar{\mathbf{v}} = \frac{\omega_\theta}{r} v_r \bar{\mathbf{e}}_\theta$$

$$\text{Q: } \frac{\partial \omega_\theta}{\partial t} + v_r \frac{\partial \omega_\theta}{\partial r} + v_z \frac{\partial \omega_\theta}{\partial z} - \frac{\omega_\theta}{r} v_r = 0 \Rightarrow \frac{\partial}{\partial t} \left(\frac{\omega_\theta}{r} \right) + v_r \frac{\partial}{\partial r} \left(\frac{\omega_\theta}{r} \right) + v_z \frac{\partial}{\partial z} \left(\frac{\omega_\theta}{r} \right) = 0$$

↓
DIVIDING BY r

Consider the planar inviscid flow of a constant density fluid through a contraction in a channel. The velocity profile upstream from the contraction (i.e. as $x \rightarrow -\infty$ for $0 \leq y \leq H_1$) is given by $\mathbf{v} = U_1(y)\mathbf{e}_x = Ay\mathbf{e}_x$ and the pressure is $p = p_1$, where A and p_1 are constant. Obtain the velocity profile $\mathbf{v} = U_2(y)\mathbf{e}_x$ and the pressure $p = p_2$ downstream from the contraction (i.e. as $x \rightarrow +\infty$ for $0 \leq y \leq H_2$).



$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial y}$$

$$x \rightarrow -\infty, 0 < y < H_1: u = U_1(y), v = 0$$

$$x \rightarrow +\infty, 0 < y < H_2: \frac{\partial u}{\partial x} = 0, v = 0$$

$$-\infty < x < \infty: y = 0: v = 0$$

$$y = h(x): \mathbf{v} \cdot \mathbf{n} = 0 \Rightarrow$$

$$u \frac{dh}{dx} = v$$

$$\int_0^{h(x)} \frac{\partial u}{\partial x} dy + v(x, h) - v(x, 0) = 0 \Rightarrow \frac{d}{dx} \int_0^h u dy - \frac{dh}{dx} u(x, h)$$

$$\Rightarrow \frac{d}{dx} \int_0^h u dy = 0 \Rightarrow$$

$$\int_0^h u dy = \int_0^{H_1} u_1 dy$$

$$\mathbf{v} \cdot \nabla \left(\frac{u^2 + v^2}{2} + \frac{p}{\rho} \right) = 0 \Rightarrow$$

$$\frac{u^2 + v^2}{2} + \frac{p}{\rho} = C$$

$$\frac{p_2}{\rho} + \frac{U_2^2(y)}{2} = \frac{p_1}{\rho} + \frac{U_1^2(y_0)}{2} \Rightarrow$$

$$U_2 = \sqrt{U_1^2(y_0) + 2 \frac{p_1 - p_2}{\rho}}$$

$$U_1 dy_0 = U_2 dy \Rightarrow$$

$$dy =$$

$$\frac{U_1(y_0) dy_0}{\sqrt{U_1^2(y_0) + 2 \frac{p_1 - p_2}{\rho}}}$$

$$\Rightarrow H_2 = \int_0^{H_1} \frac{U_1(y_0) dy_0}{\sqrt{U_1^2(y_0) + 2 \frac{p_1 - p_2}{\rho}}}$$

$$y = \int_0^{y_0} \frac{U_1(y_0) dy_0}{\sqrt{U_1^2(y_0) + 2 \frac{p_1 - p_2}{\rho}}}$$

PROVIDES $\frac{p_1 - p_2}{2 \frac{\rho}{\rho}}$

PROVIDES $y(y_0)$

$$U_2 = \sqrt{U_1^2(y_0) + 2 \frac{p_1 - p_2}{\rho}} \rightarrow \text{GIVES } U_2(y)$$

For $U_1 = Ay_0 \rightarrow y = \int_0^{y_0} \frac{U_1(y_0) dy_0}{\sqrt{U_1^2 + \frac{2(p_1 - p_2)}{\rho}}}$ $\Rightarrow y = \sqrt{y_0^2 + \frac{2(p_1 - p_2)}{\rho A^2}} - \sqrt{\frac{2(p_1 - p_2)}{\rho A^2}}$

$y = H_2$
 $y_0 = H_1 \rightarrow \boxed{\frac{2(p_1 - p_2)}{\rho A^2} = \left(\frac{H_1^2 - H_2^2}{2H_2} \right)^2}$ $\hookrightarrow y_0^2 = y \left(y + \frac{H_1^2 - H_2^2}{2H_2} \right)$

$\boxed{U_2 = \sqrt{U_1^2(y_0) + \frac{2(p_1 - p_2)}{\rho}} = \sqrt{A^2 y_0^2 + A^2 \left(\frac{H_1^2 - H_2^2}{2H_2} \right)^2} = A \sqrt{\left(y + \frac{H_1^2 - H_2^2}{2H_2} \right)^2} = A \left(y + \frac{H_1^2 - H_2^2}{2H_2} \right)}$

THE SOLUTION CAN ALSO BE OBTAINED ^{FROM ABOVE} BY NOTING THAT

$\vec{v} \cdot \nabla w = 0 \rightarrow w = w(p) = -A = \frac{\partial v}{\partial y} - \frac{\partial u}{\partial x}$

As $y \rightarrow \infty \rightarrow u \rightarrow 0 \rightarrow u = Ay + C$

USING CONTINUITY $\int_0^{H_1} Ay dy = \int_0^{H_2} (Ay + C) dy \rightarrow \boxed{C = \frac{A}{2} \frac{H_1^2 - H_2^2}{H_2}}$

USING BERNOULLI ALONG ANY STREAMLINE DETERMINES

$\frac{p}{\rho} + \frac{U^2}{2} = Cp$

$\boxed{\frac{p_1 - p_2}{\rho} = \frac{C^2}{2} = \frac{A^2}{2} \left(\frac{H_1^2 - H_2^2}{2H_2} \right)^2}$